# CEMHYD3D: Overview and Current Status

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#### **Model Characteristics**

- Three-dimensional (100 μm on a side)
- Multi-size, multi-phase cement particles
  - representative of real cement of interest
- silica fume, fly ash (future- slag, kaolin)
- gypsum, hemihydrate, and/or anhydrite sulfate sources
- simulates dissolution, diffusion, & reaction



# Inputs to CEMHYD3D

- Cement (mineral admixture) particle size distribution
- cement bulk composition and surface composition
- apparent activation energies for cement and mineral admixtures
- volume fraction of aggregates
- curing conditions
  - isothermal/ adiabatic/ temperature profile
    - maturity method principles
  - saturated/ sealed/ drying
    - self-desiccation and creation of "empty" porosity



# **Outputs from CEMHYD3D**

- Degree of hydration vs. time
  - all phase volume fractions
- chemical shrinkage vs. time
- heat release vs. time
  - adiabatic heat signature
- compressive strength (Power's gel-space ratio)
- diffusivity (w/c,  $\alpha$ ,  $V_{agg}$ ,  $M_{SF}$ )
- percolation of porosity (CH) -- durability
- percolation of solids -- setting
- ITZ microstructure
  - phase fractions vs. distance from aggregates



# **Model Usage**

- Academia (education and Ph. D. research)
  - U.S. (ACBM, UC Berkeley, Georgia Tech, Tennessee Tech)
  - France (Cachan)
  - The Netherlands (Twente)
  - Denmark (Technical University of Denmark)
  - Japan (Tokyo Institute of Technology)
  - China
  - South Africa (Capetown)





# **Model Usage**

- Industry
  - Germany (Dyckerhoff Zement)
  - France (CSTB)
  - The Netherlands
- Government
  - Waterways Experiment Station





# **Studies to Date Using Model**

- Calibration/Prediction studies
  - heat release and adiabatic heat signature
  - degree of hydration
  - chemical shrinkage
  - compressive strength
- Effects of cement PSD on properties
  - coarser cements for low w/c ratio concretes
  - early age autogenous properties and cracking





# **Heat of Hydration**

- Determine heat of hydration by monitoring how much of each phase reacts/forms during each cycle
- Base results on heats of formation of each compound or on measured heats of hydration of phases

•	Compound	Heat of Hydration

•	$C_3S$	517 J/g
_	$C_3D$	JIIJg

• 
$$C_2S$$
 262 J/g

• 
$$C_3A$$
 1144 J/g

• 
$$C_4AF$$
 725 J/g

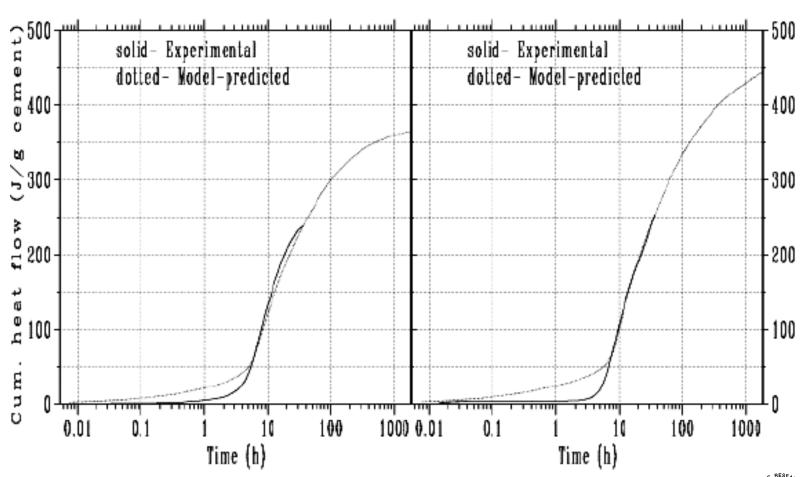
- Taylor, H.F.W., Cement Chemistry, 1992.
- Fukuhara et al., Cem Concr Res, 11, 407-414, 1981.



# **Heat of hydration**







#### **Temperature Calculation for Adiabatic Conditions**

 Update heat released and heat capacity after each cycle of hydration model and calculate T rise via:

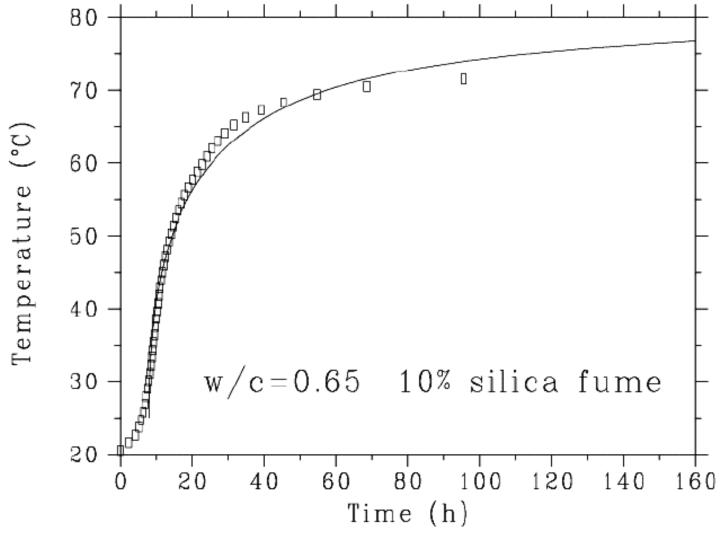
$$- \Delta T = [H(I)-H(I-1)]/C_p(I)$$

- H(I) is heat released through cycle I
  - H(I) is based on heats of reaction of clinker phases
- C<sub>p</sub>(I) is heat capacity of concrete after cycle I
  - heat capacity adjusted for imbibition of water into cement paste and conversion of free to bound water





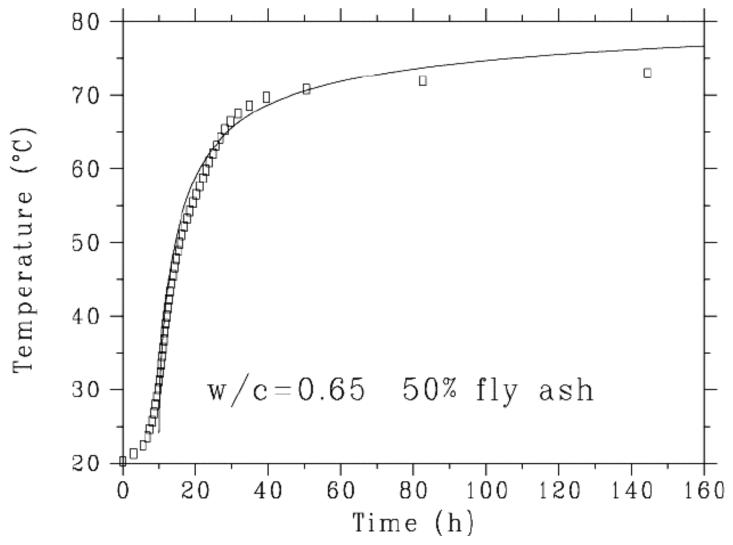
### Predicted Adiabatic Heat Signature







#### Predicted Adiabatic Heat Signature







#### **Prediction of Compressive Strength**

 Use gel-space ratio theory of Powers and Brownyard

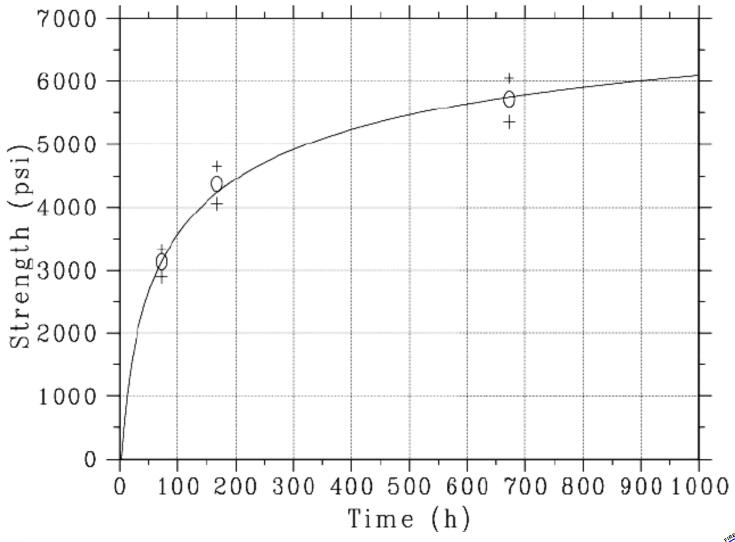
$$-X = (0.68 * \alpha)/(0.32 * \alpha + w/c)$$
$$-\sigma_c = A * X^n \qquad (n=2.6 \text{ to } 3.0)$$

- Calibrate A via measured 3-day compressive strength (assume n=2.6)
- Use hydration model to predict X vs. time and calculate 7-day and 28-day compressive strengths to compare to experiment





# **Compressive Strength Prediction**







# **Cement PSD and Properties**

- Cement finenesses have increased dramatically from the 1950's (250-300 m<sup>2</sup>/kg) to present date (350-400 m<sup>2</sup>/kg)
- High performance concrete mixture proportions substantially different from conventional ones (lower w/c ratio, silica fume, etc.)
- Question: Have cements been optimized for HPC mixture proportions? --> CEMHYD3D





# **Systems Examined**

Clinker ground to different finenesses

$$-$$
 <5  $\mu$ m> 643 m<sup>2</sup>/kg <10  $\mu$ m> 520 m<sup>2</sup>/kg

$$- < 15 \mu m > 387 \text{ m}^2/\text{kg} < 20 \mu m > 296 \text{ m}^2/\text{kg}$$

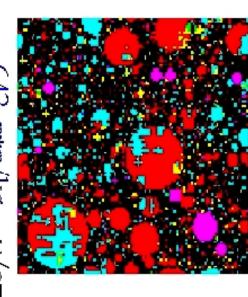
$$-$$
 <25 µm> 254 m<sup>2</sup>/kg <30 µm> 212 m<sup>2</sup>/kg

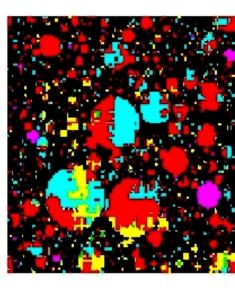
• Composition: C<sub>3</sub>S- 56.3 %, C<sub>2</sub>S- 24.7 %, C<sub>3</sub>A- 0.6 %, C<sub>4</sub>AF- 13.5 %, Hemi- 4.6-5 %





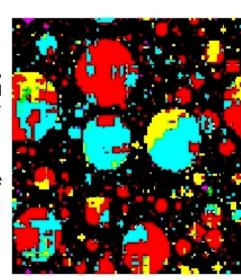
# 2-D slices from initial 3-D cement microstructures

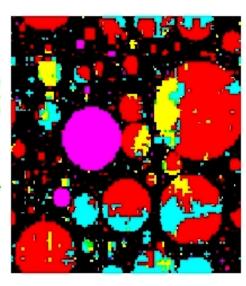




643 m\*m/kg w/c=0.35

387 m\*m/kg





254 **m\*m/**kg

212 **⊪™**/kg

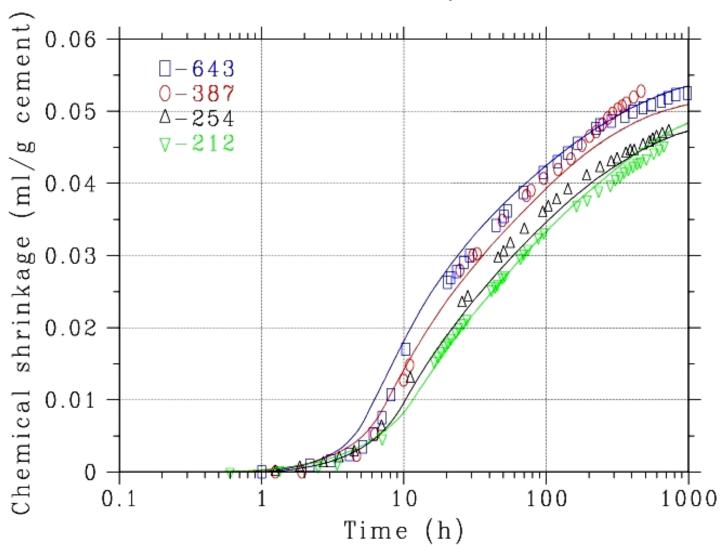
Note the increase in particle spacing (pore size) for the two coarser cements (254 and 212)





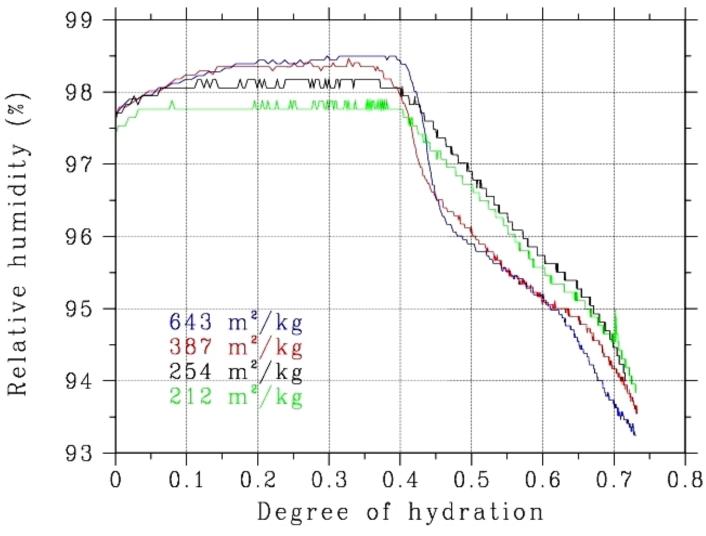
# **Chemical Shrinkage**

time=0.125\*cycles





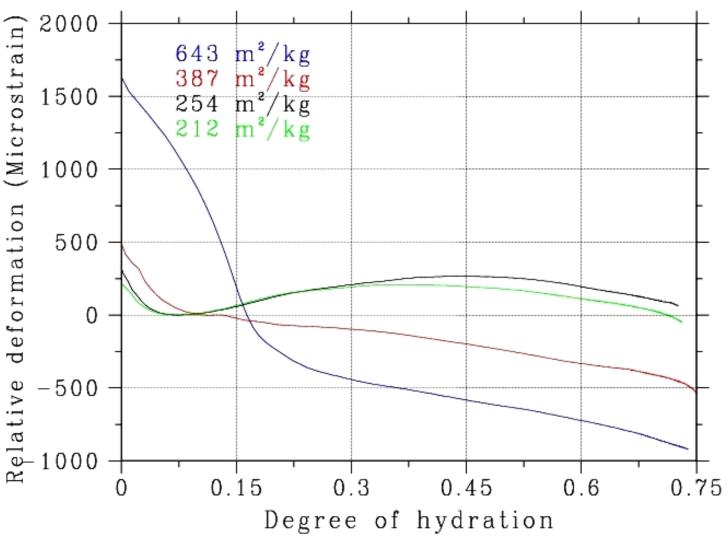
# **Internal Relative Humidity**







# **Autogenous Shrinkage**







#### **Conclusions**

- In HPCs, coarser cements:
  - reduce early hydration and heat release (and strength!)
  - enhance "curability" by shifting depercolation of capillary porosity to lower values
  - increase diffusivities at early times, but result in equivalent diffusivities at longer times (equivalent hydration)
  - reduce internal RH reduction and autogenous strains and stresses





# What's missing?

- Better modeling of influence of sulfate
  - work in progress with Dyckerhoff Zement
- Modeling of influence of alkalies
  - some work done for a Ph. D. in The Netherlands
- Modeling of slag, kaolin, others
  - ongoing experimental studies to clarify mechanisms and reactions
- Modeling of influence of specific chemical admixtures

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